

QCM Accelerator Structure ESRF CDR Contribution

21 April 2026

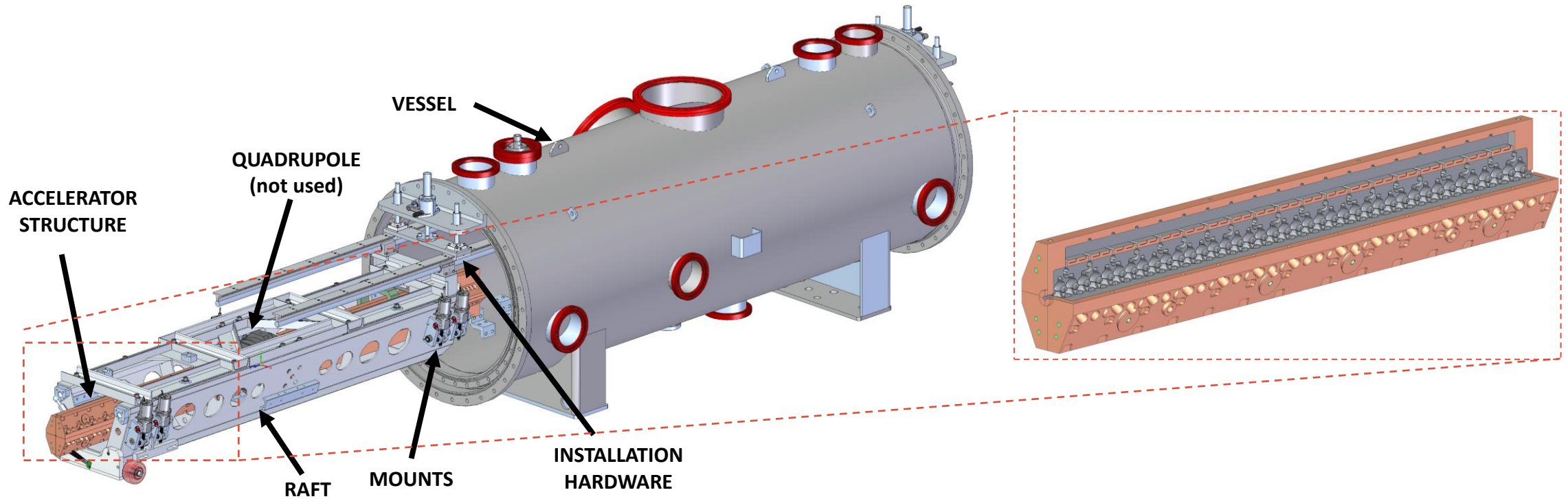
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Agenda

1. QCM Overview
2. Schedule
3. Accelerator RF Design
4. QCM Design and Build Status
5. Alignment Requirements
6. External Mounts
7. Cryogenic Requirements
8. Vacuum Requirements

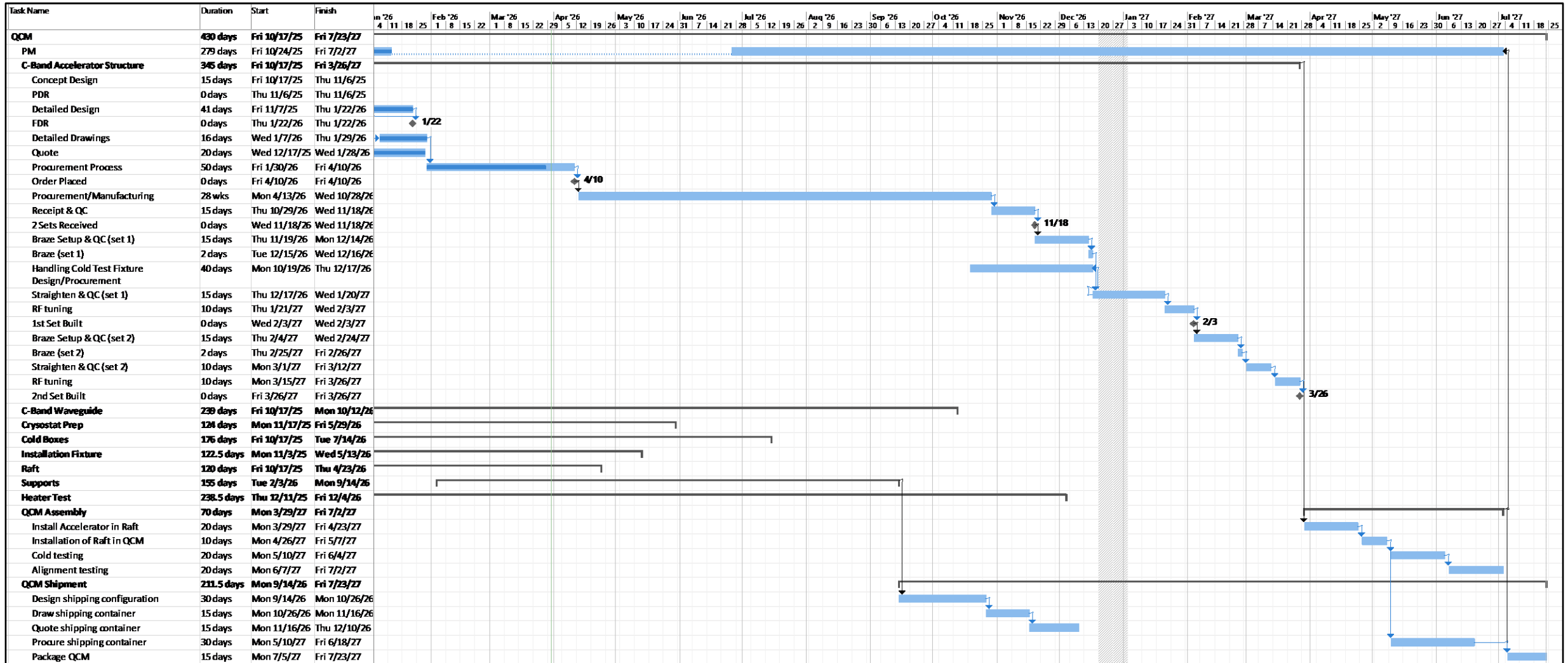
QCM Overview

- Original goal: demonstrator for C³
- Additional goal: provide QCM to ESRF
 - The full C³ design works for ESRF, but ESRF has less stringent requirements



Proposed Schedule

- Mechanical assembly of the QCM to start by Nov 2026, allowing testing before shipment to ESRF by July 2027



Procurement Status

Long Lead Items

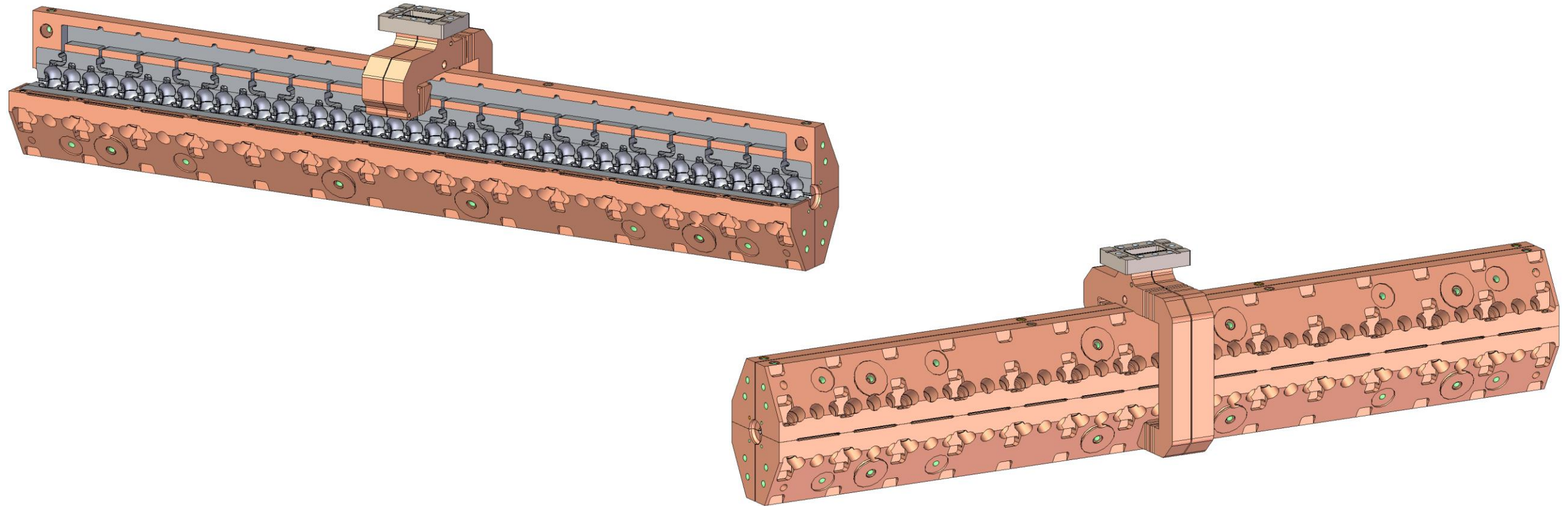
Accelerator Structure

- Request for Proposal process completed via Sam.gov website – received 8 bids
- A vendor has been identified, but paperwork and contracts are still in process
- Lead time for the first set of parts is 28 weeks and for the complete two sets of parts is 34 weeks.
 - Receive at SLAC in November 2026

Cryomodule

- Received at SLAC in 2025

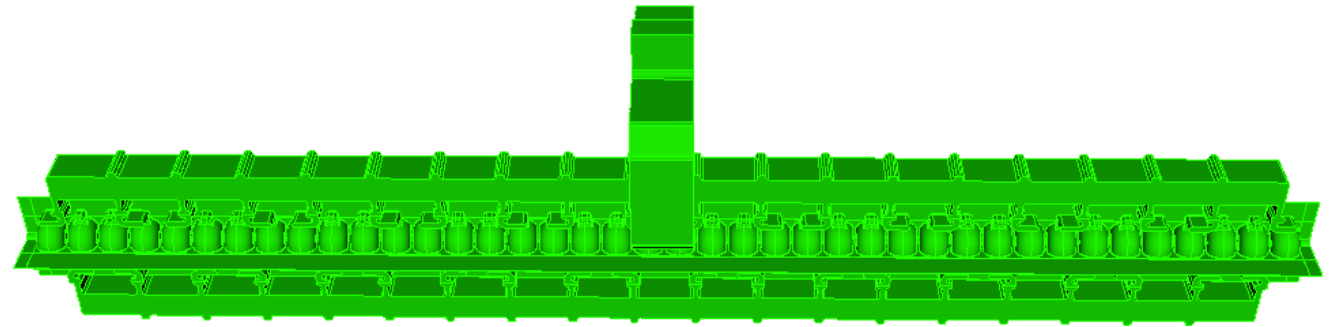
Design and Build Status – Accelerator Structure



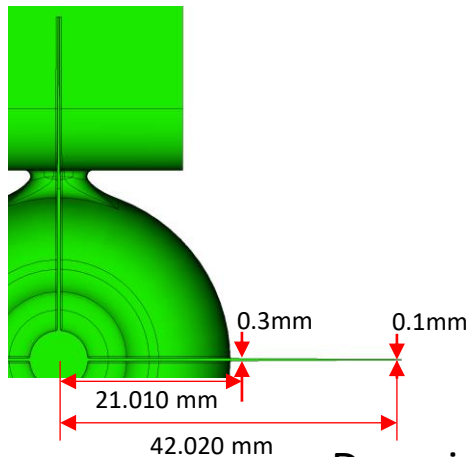
Final RF Geometry

Features

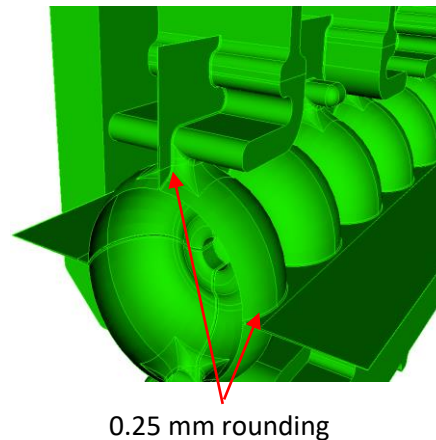
- 40 cells with pair wise side to side distributed coupling
- Cell Balancing features
- 4 damping slots extending to the beam center line (4 part open cells and iris)
- Structures to be spaced so that cell center to center distance is $(N+.5)*26.242$ at operating temperature



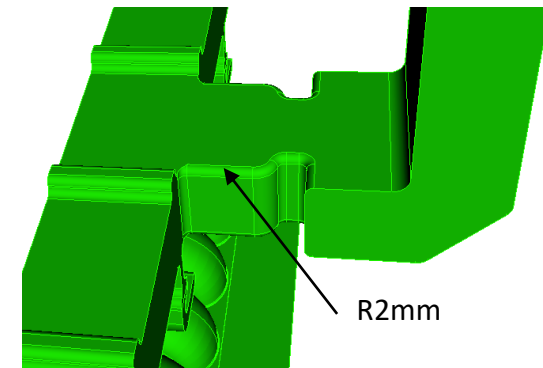
1-m structure: 40-cell with damping slots



Damping slot



0.25 mm rounding

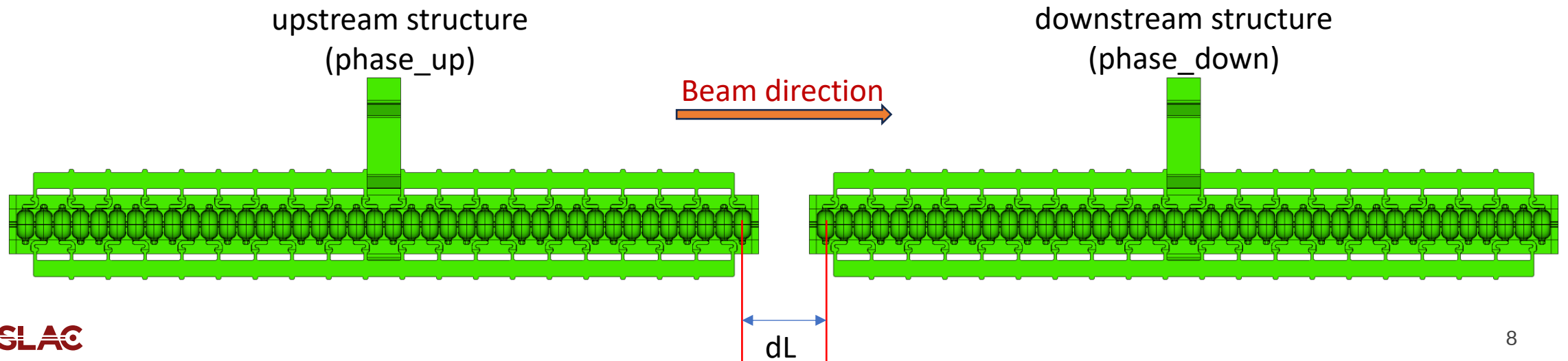


Waveguide corner rounding

Final RF Geometry

Position and RF Phasing Two or More C-Band Structures to Cancel Backward Acceleration

- C-Band PI-mode cell length $L_{\text{cell}} = 26.242$ mm
 - Separation required to cancel acceleration: dL
 - Measured from center to center of two end cells
 - $dL = (n + 1 + 0.5) * L_{\text{cell}}$
 - $n = 0, 1, \dots$
 - Structure RF phase
 - $\text{phase_down} - \text{phase_up} = -(n+0.5) * 180$ degree
- Note: all dimension measured at operating temperature applies to more than two structures

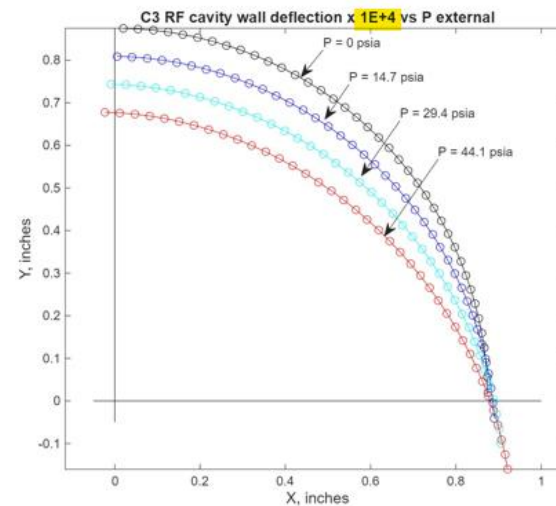
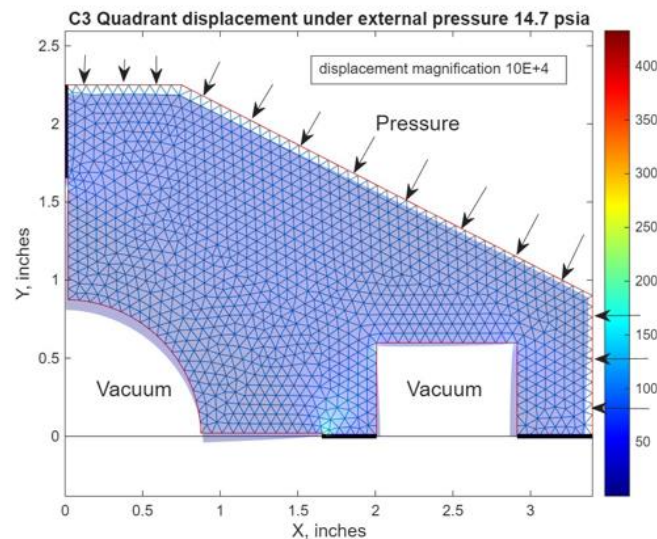


FEA: Deflection Under Pressure, 2D

The “2r” wide damping slots create continuous vacuum space that must be supported to prevent excessive displacement of the cell surfaces. Small predictable elastic deformation can be compensated for during structure tuning.

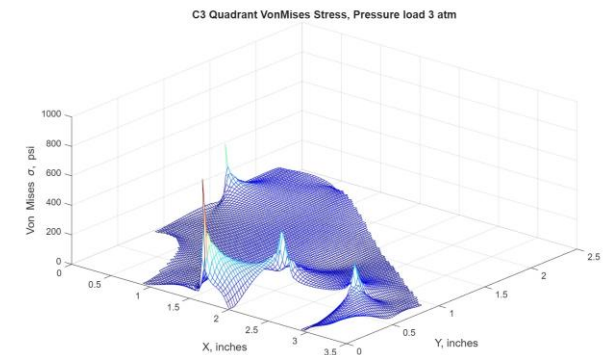
This was initially reviewed with simplified geometry in 2D to determine if the span would need support within the damping slots or if the full span could be supported by the structure.

With distortion in the range of .3 μ m conclusion is that the damping slots can remain continuous without interruption for support as long as the inner WG joint is well connected.



- The motion of the upper end of the cavity wall under external pressure in microns is:

P	Ux	Uy	U
14.7	-.036	-.167	.171
29.4	-.073	-.334	.341
44.1	-.109	-.500	.513



FEA: LN Pool Boiling

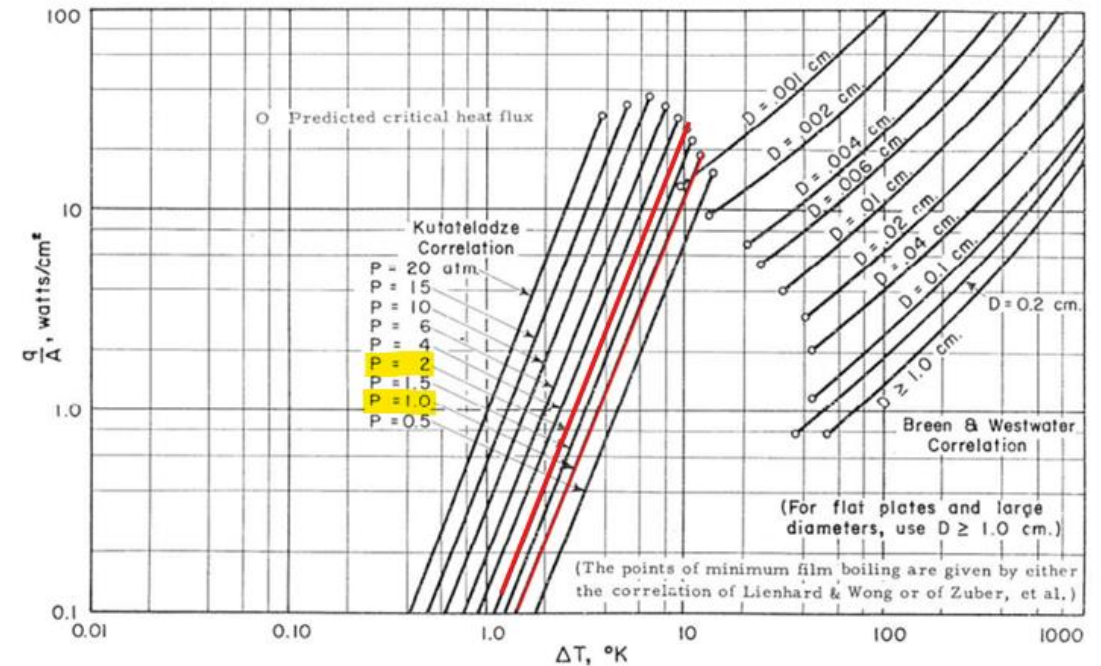
Chart shows heat transfer coefficient in nucleate and film boiling regimes as well as transition temperatures. **The design goal is to avoid film boiling, staying in nucleate boiling.**

To remain in nucleate boiling (at nitrogen pressures between 1 and 2 atm) the **surface/bulk temperature difference must remain below ~10 K.**

In nucleate boiling the heat transfer coefficient will vary from ~.1 to 10 W/cm² as the surface/bulk temperature difference ranges from ~1 to 10K. (.1 to 1 W/cm²/K)

Other sources were checked with similar coefficients. **Simulations indicate that this is not critical as the surface heat flux is well below onset of film boiling.**

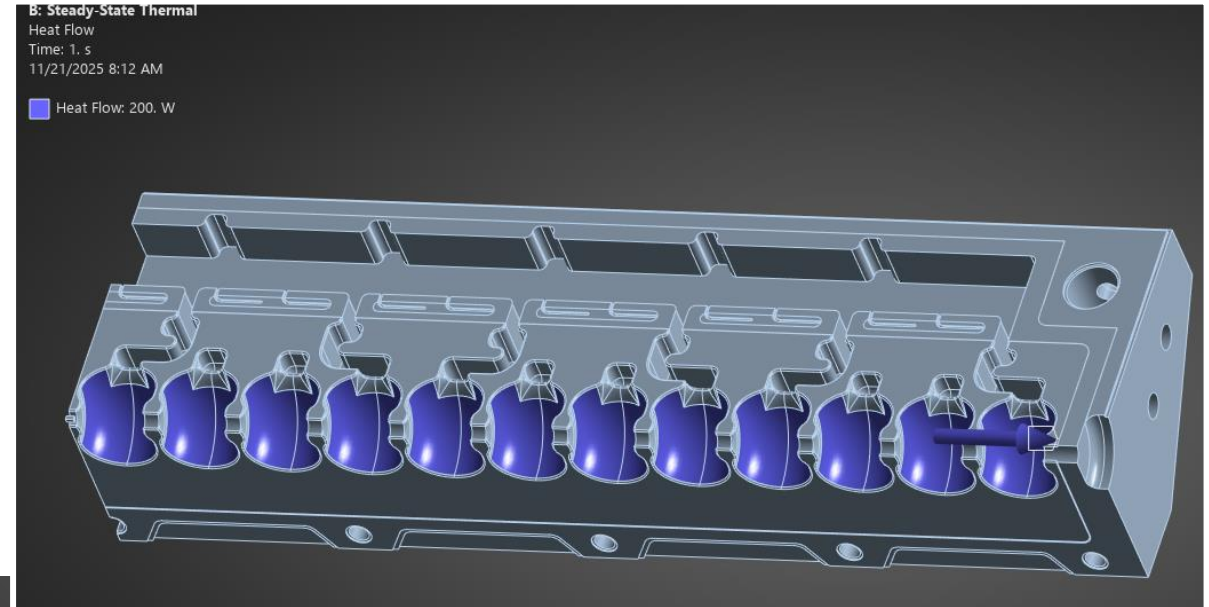
Prediction of Nucleate/Film Boiling for Nitrogen



FEA: Structure Cooling

Our typical (and proposed) tuning features create 2 potentially problematic conditions.

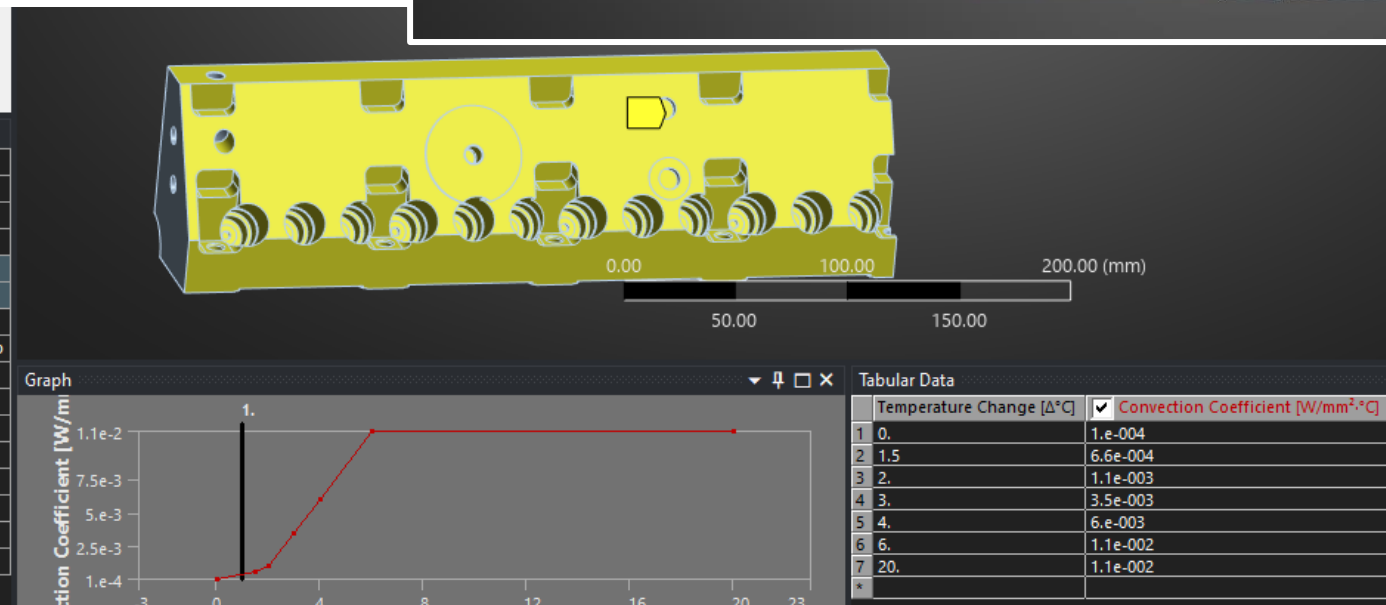
- Gas trapped areas that will not be well cooled
- Areas close to the cell walls that may flash to film boiling



Imported Load (B6)
Solution (C6)
Solution Information
Directional Deformation Y

Details of "Convection-allExt"

Scope	
Scoping Method	Geometry Selection
Geometry	203 Faces
Definition	
ID (Beta)	95
Type	Convection
Film Coefficient	Tabular Data
Coefficient Type	Difference of Surface and Bulk Temp
Ambient Temperature	-198. °C (ramped)
Convection Matrix	Program Controlled
Suppressed	No
Edit Data For	Film Coefficient
Tabular Data	
Independent Variable	Temperature
Graph Controls	
X-Axis	Temperature



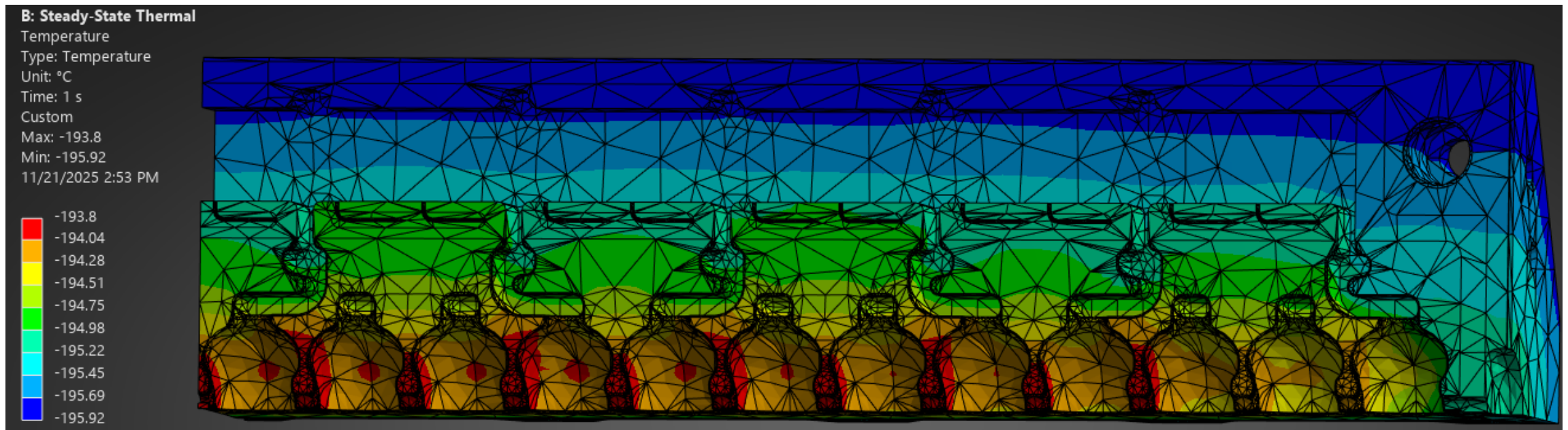
- Used 12 cells and included "end effect"
- Loss then $2500/40 * 12/4 = 187 >$ round up to 200 W
- Cooling ranged from all exterior to just the main faces
- Used convection coeff from ~relevant sources

FEA: Pool Boiling Temperatures

Case with no cooling at the tuner surfaces indicates inside temperatures at approximately 4° above the LN bulk temperature.

As this is “well below” the film transition temperature of ~10°, no modification of the tuning features is thought essential.

- This also shows the extent of the additional end cooling which is discussed on subsequent slides.



FEA: Heat Transfer, Pressure, & End Effects

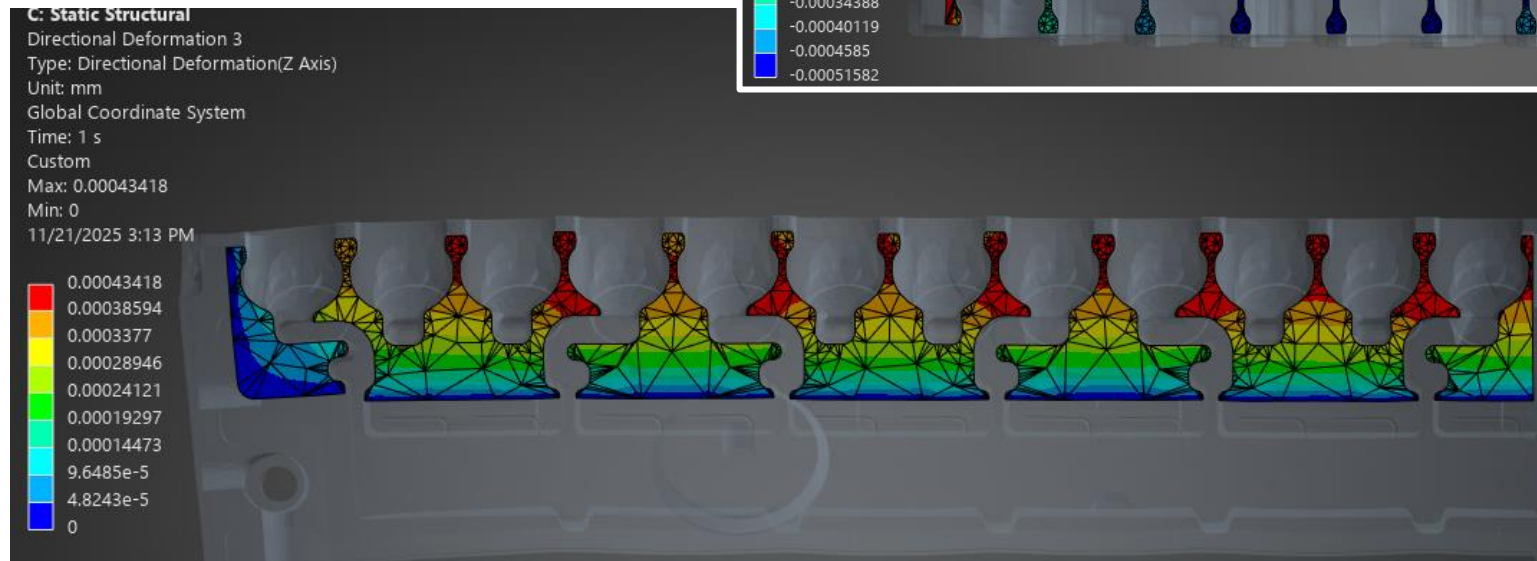
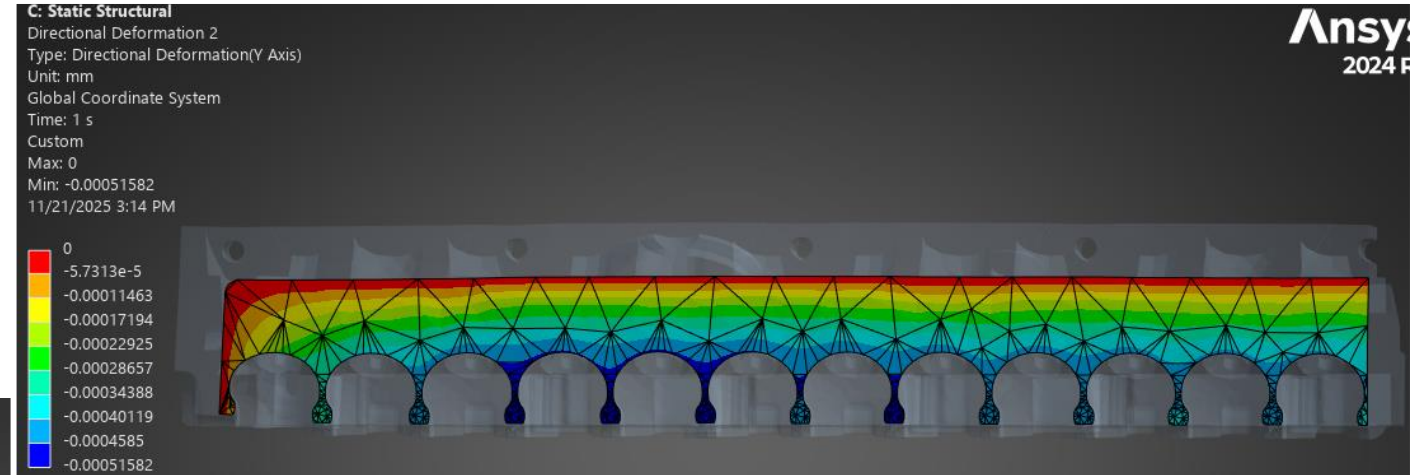
Deformation normal to the damping slot

Distortion from RF heating and 3 atm pressure
(1.5x design)

Case without any tuner surface heat transfer

Displacement of less than $0.5 \mu\text{m}$ is acceptable

Some tuning offsets to compensate for end effects may be incorporated.



Temperature (C)	Thermal Conductivity (W m ⁻¹ C ⁻¹)
-200	580
-100	413
23	397

Temperature (C)	Coefficient of Thermal Expansion (C ⁻¹)
-200	7.4E-06
-100	1.44E-05
23	1.674E-05

Temperature (C)	Young's Modulus (Pa)
-200	138000000000
-100	133000000000
23	126000000000

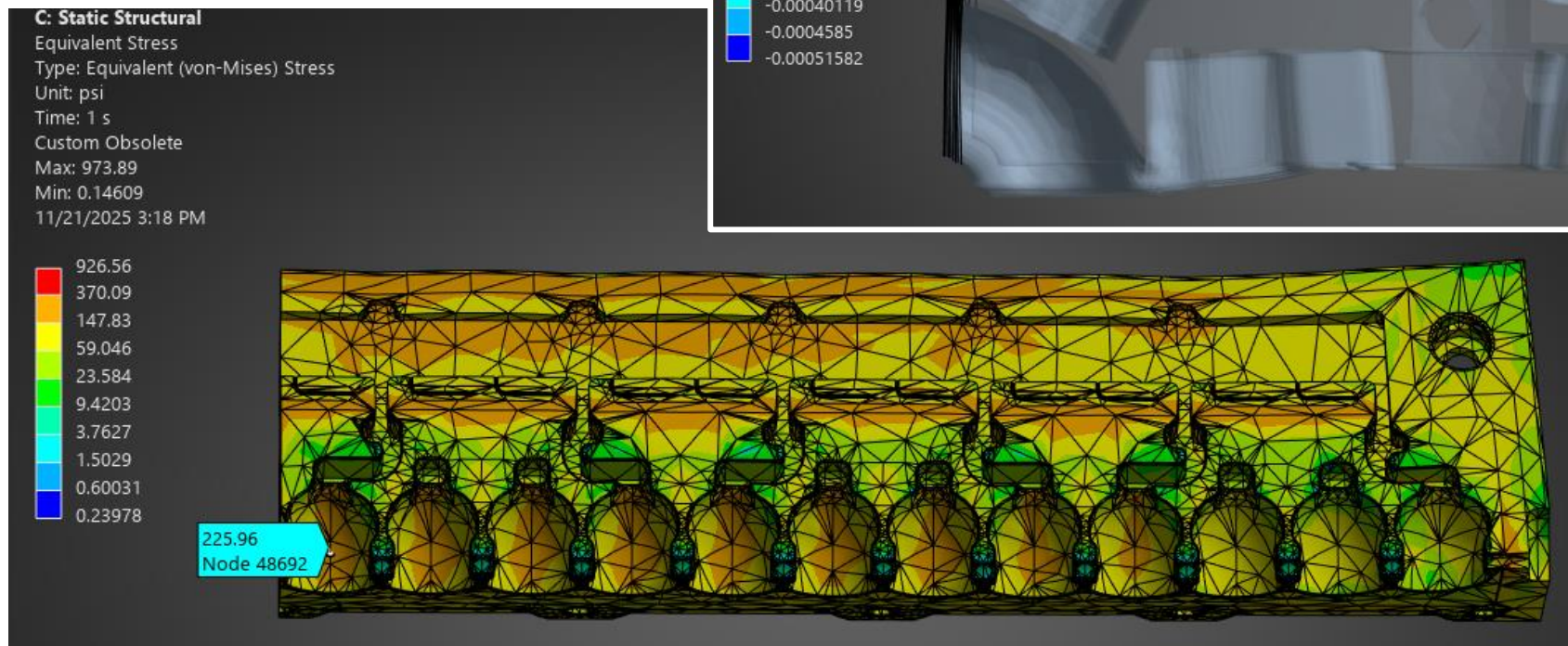
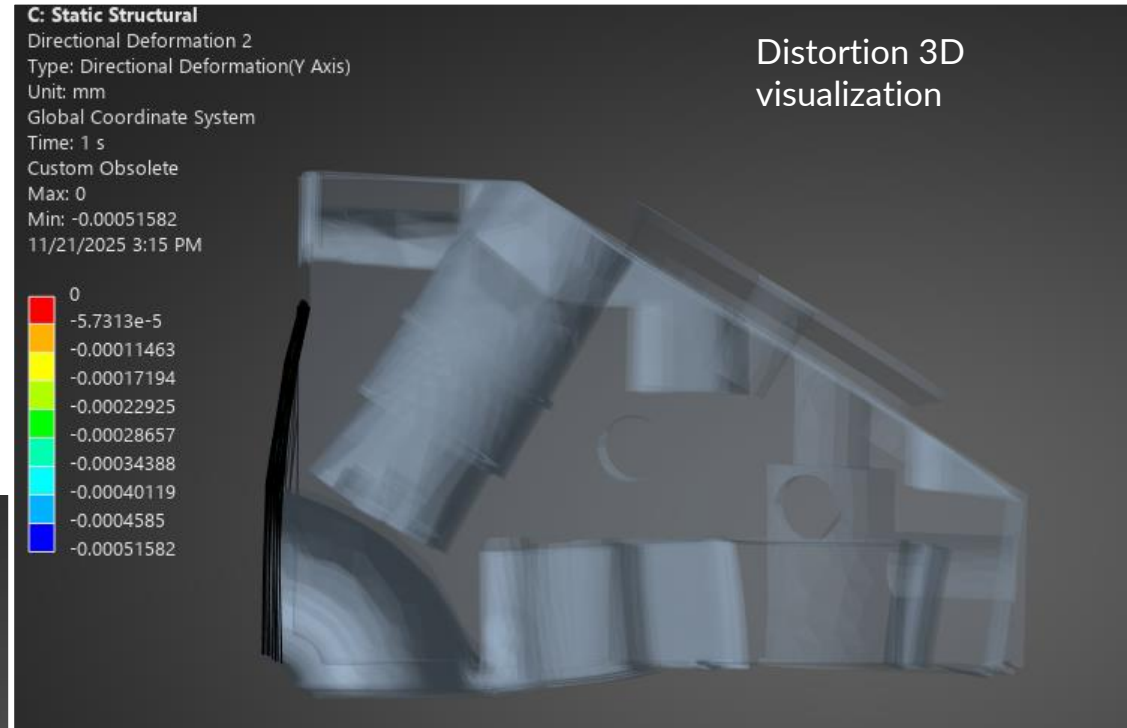
Temperature (C)	Poisson's Ratio
-200	0.338
-100	0.341
23	0.345

FEA: Heat Transfer, Pressure, & End Effects

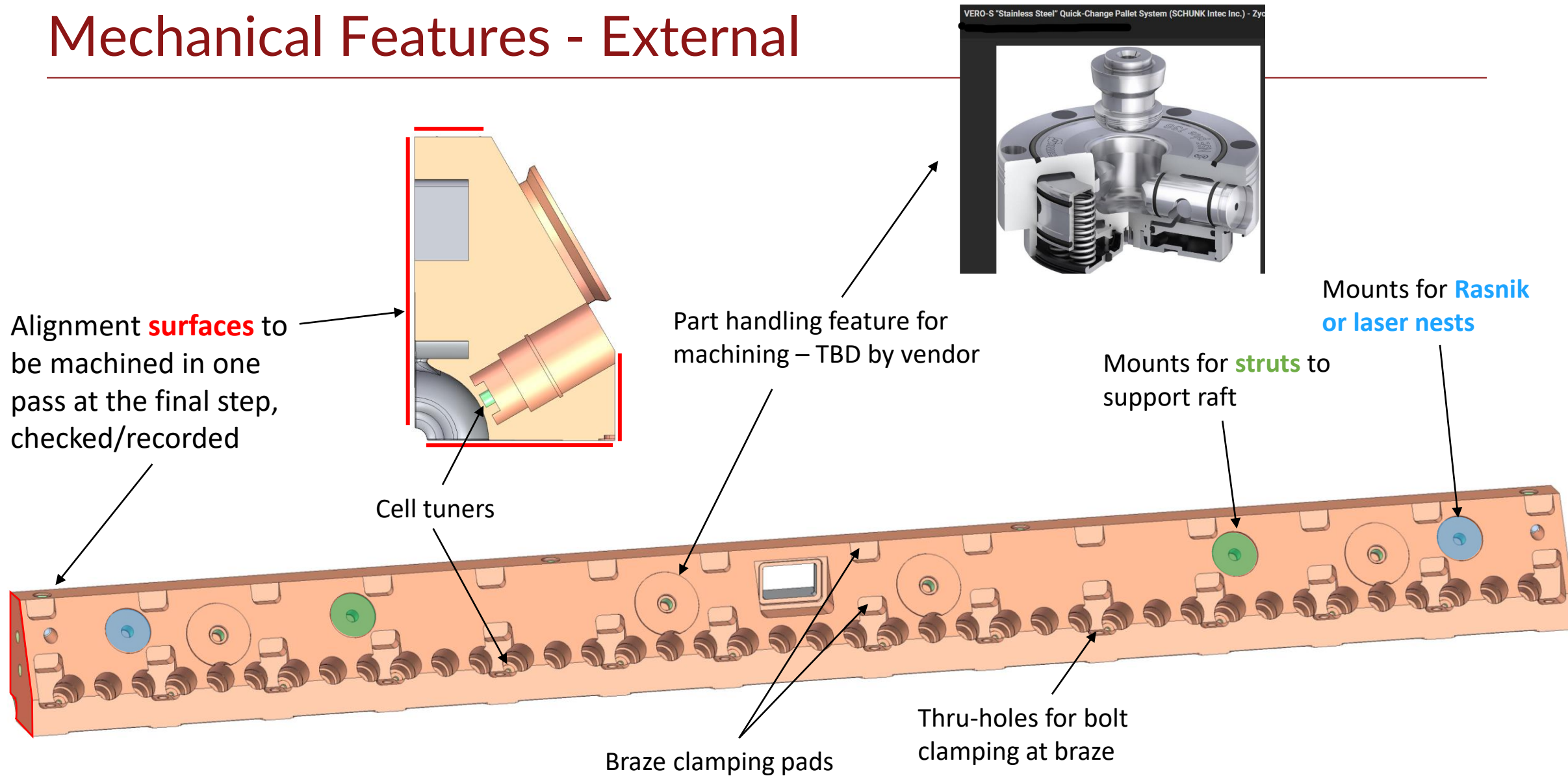
Conditions from previous slide

Von-Mises stress below 1 kpsi. Annealed copper yields at >3 kpsi.

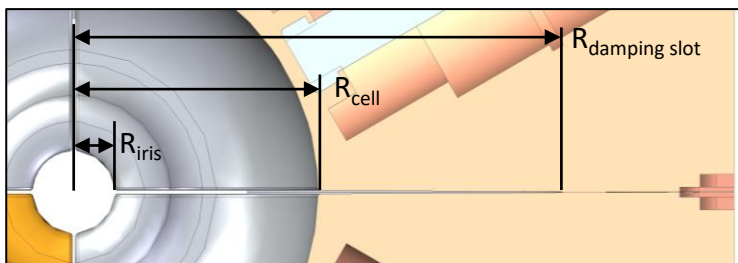
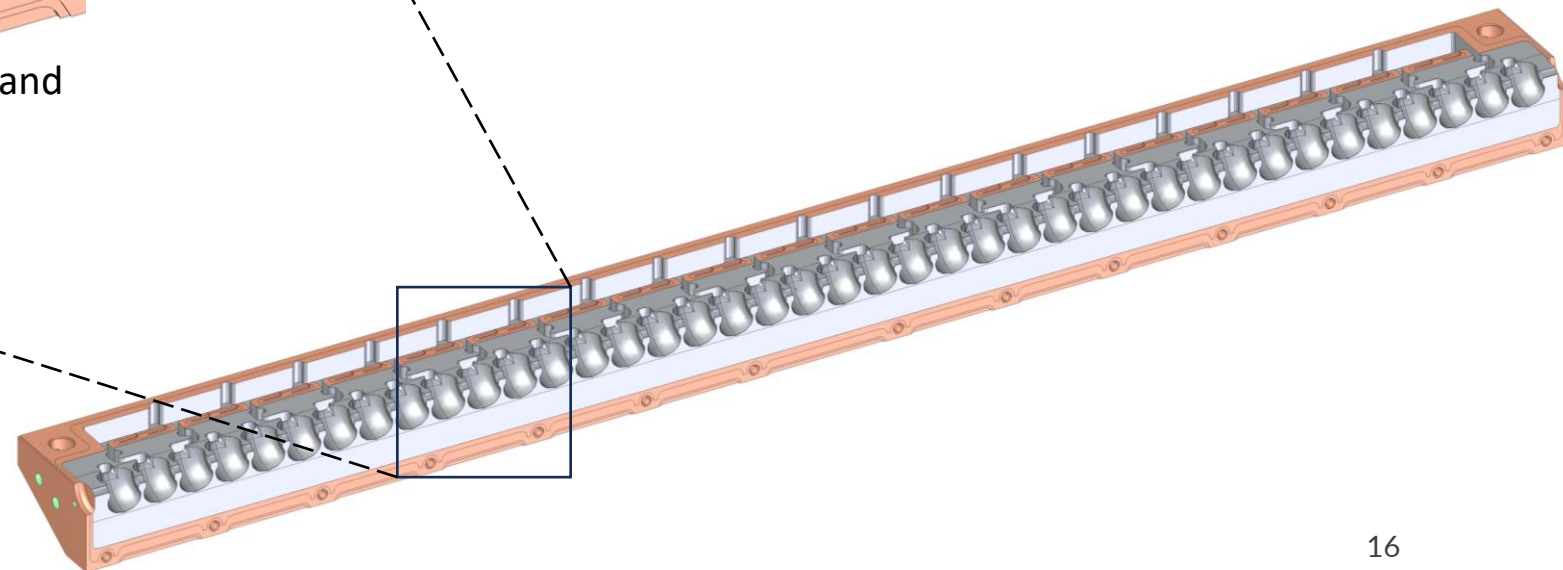
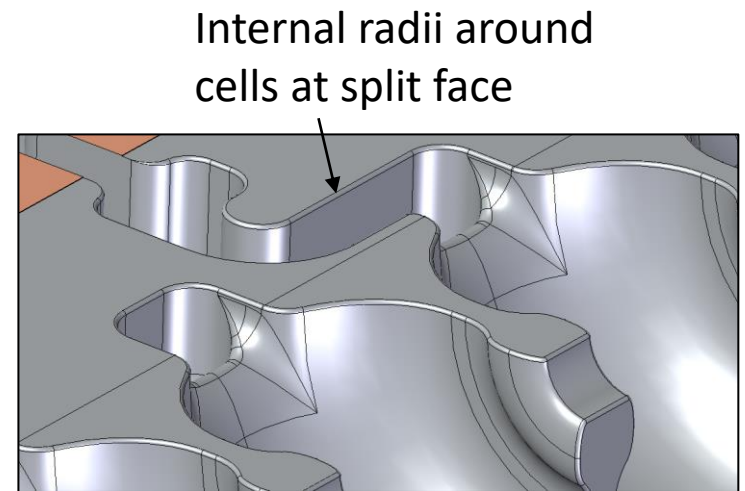
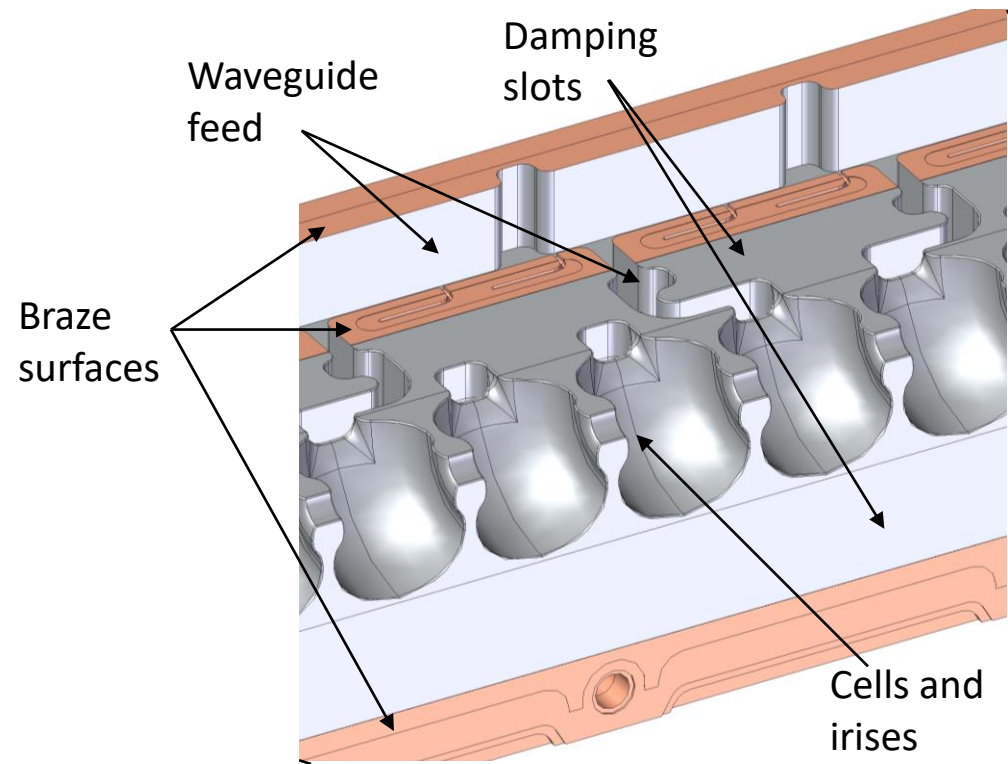
Yielding is not expected



Mechanical Features - External



Mechanical Features - Internal

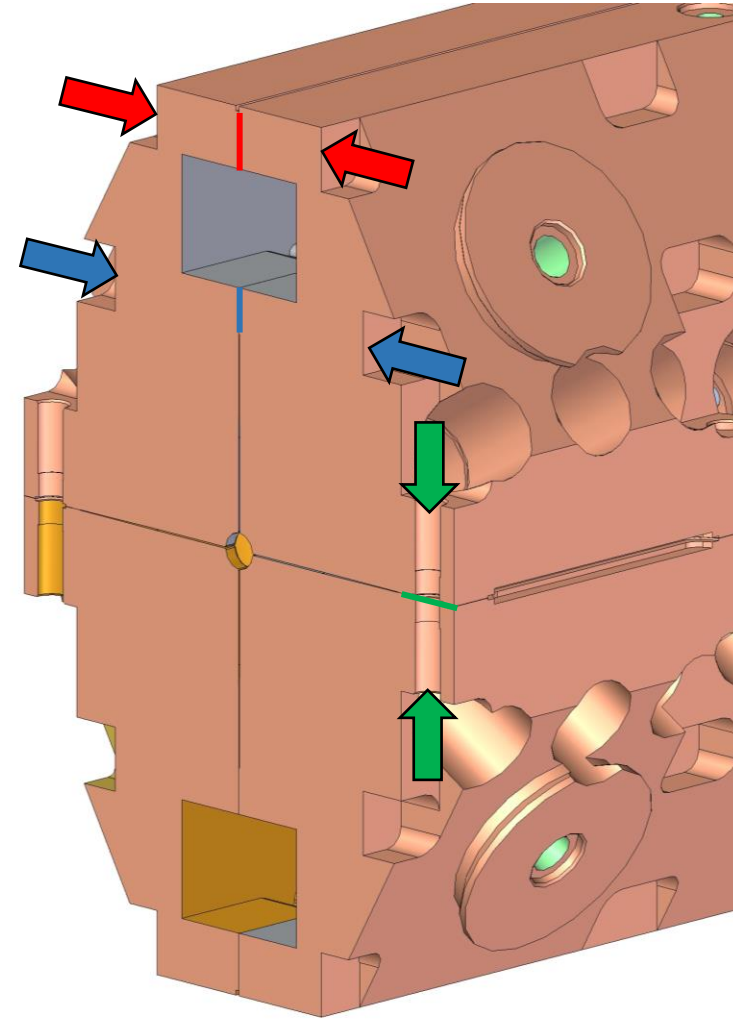
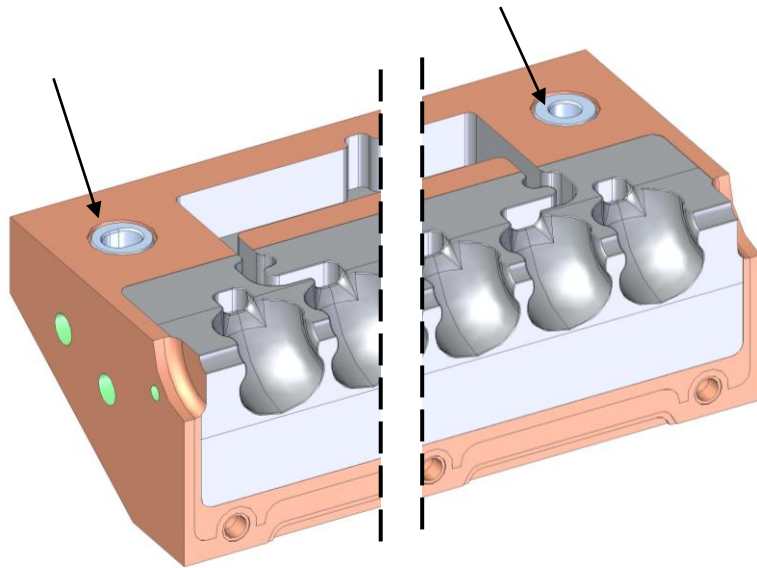


Braze Steps and Features

3 critical “perimeter” joints (2 vacuum, 1 mechanical)

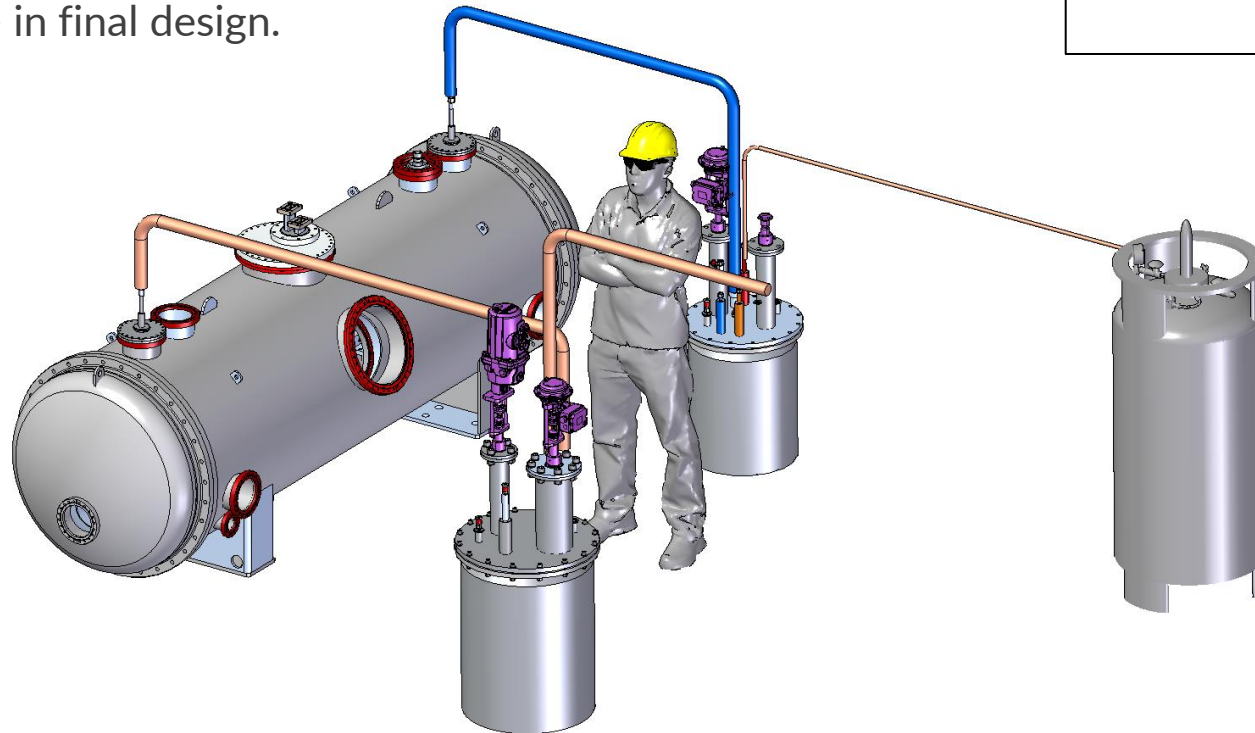
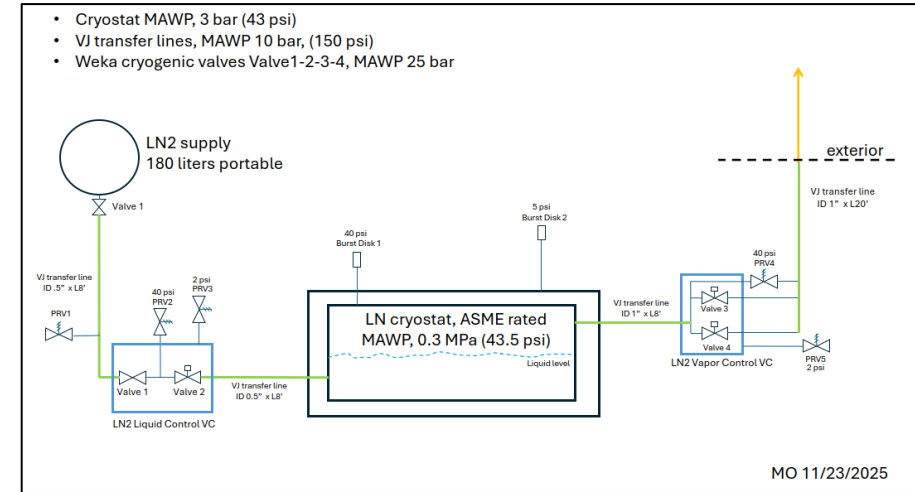
During braze, the braze joints are held by **external clamps** and **compression bolts**.

At assembly, alignment is achieved with a pin and slot arrangement, using stainless steel inserts to prevent deformation of the hole and slot (exterior flat surfaces may also be used)



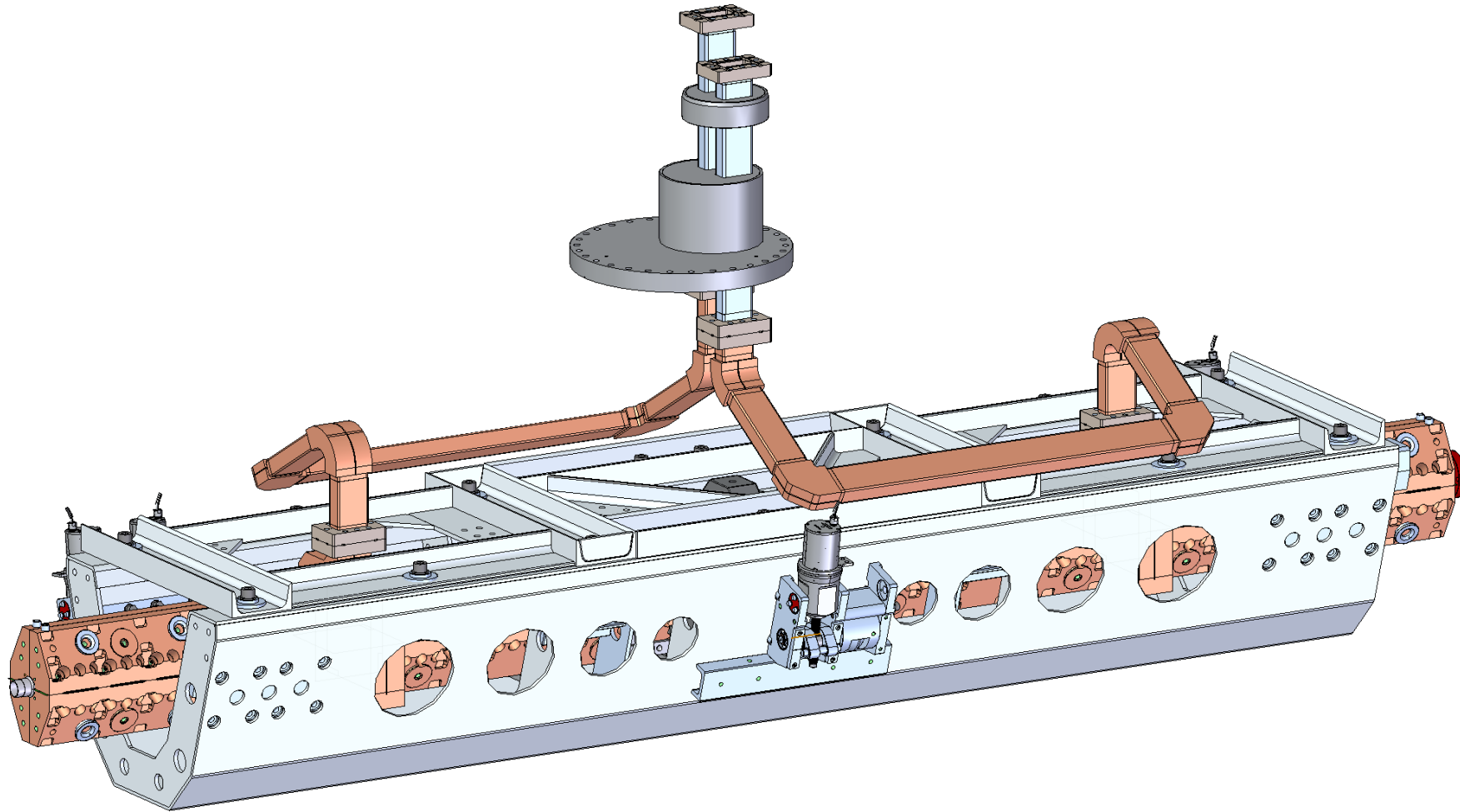
Design and Build Status – Cold Box/Fill Lines

- Cold boxes designed to enable controlled filling/venting of cryomodule.
- P&ID agreed upon with SLAC pressure vessel safety team.
- Valves are already received at SLAC.
- Half of the transfer lines and bayonets are received at SLAC, but will require additional components or modification.
- Boxes and lids are in final design.



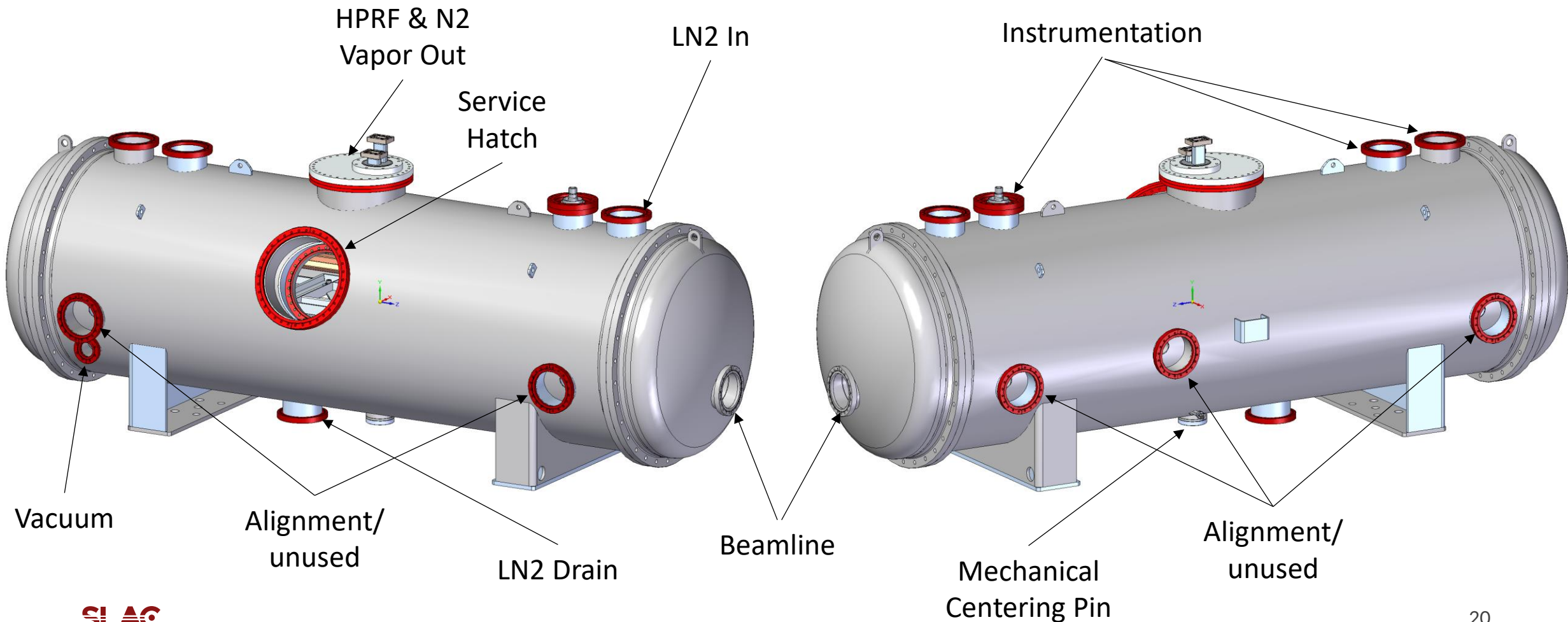
Design and Build Status – HPRF Waveguide

- Feedthrough into the QCM is via stainless steel waveguides bolted externally and internally.
- Internal waveguides are of copper and have an elongated path to make them flexible, allowing for mm-scale adjustments of the raft and accelerator while the feedthrough is fixed.



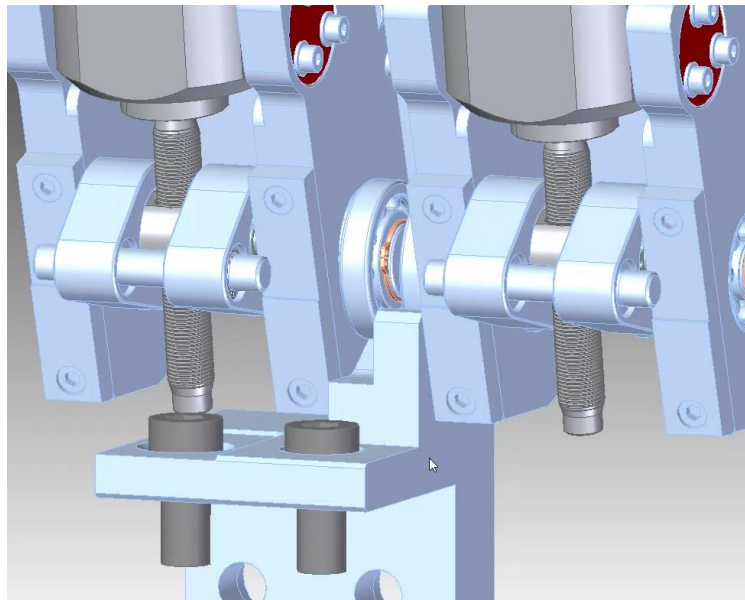
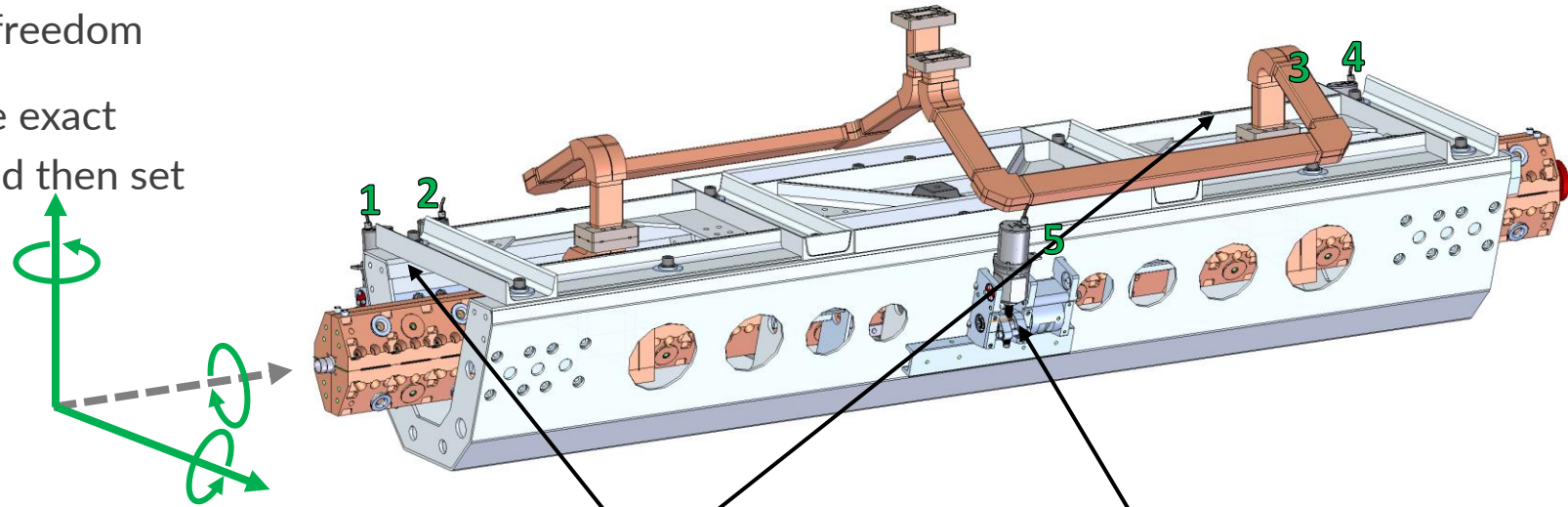
Design and Build Status - Feedthroughs

Proposed feedthrough locations

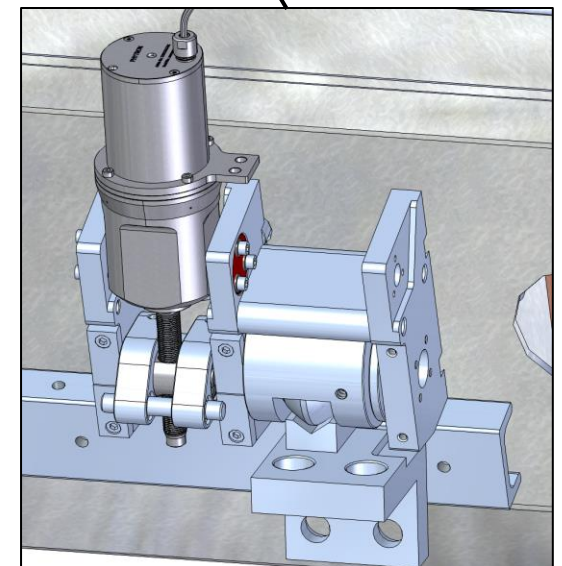
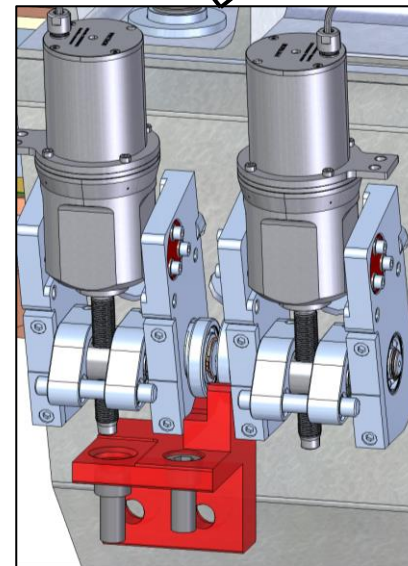


Design and Build Status – Mounts/Movers/Loaders

- 5 adjustable mounts for 5 degrees of freedom
- Adjustable range is mm-scale, with the exact limits to be agreed upon with ESRF and then set by SLAC.



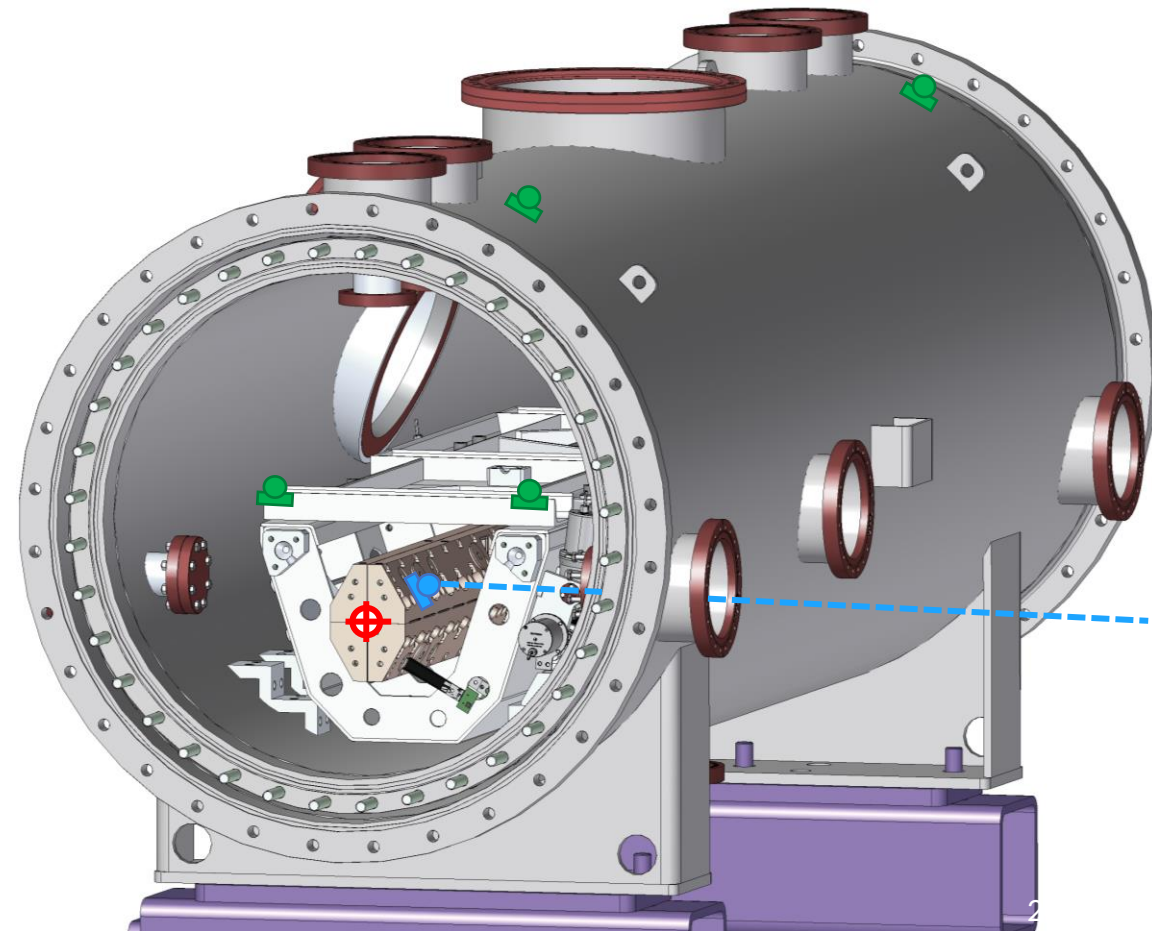
Animation showing various movements for one pair of movers



Mechanical Features – Alignment and Fiducials

ESRF needs: Precision alignment of the structures in the QCM to the machine coordinates (beam tunnel/mating components) and a means of verification/adjustment.

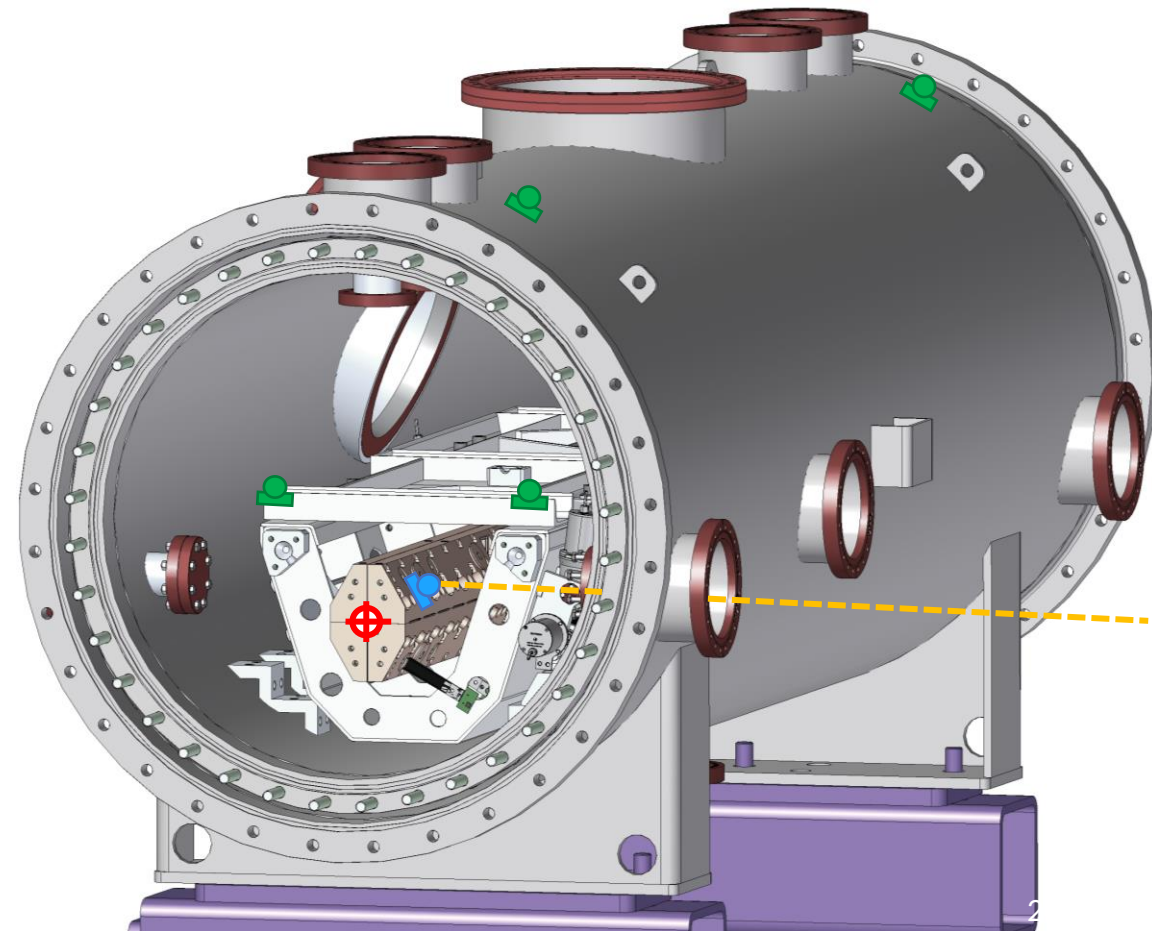
- Will want to check alignment while warm with cryovessel open – confirm if any movement during shipping.
- Needs confidence of the location while cold, however that is established.
- **Option 1:** While warm, transfer datums to external fiducials and use a calculated or empirical “cold-warm” adjustment.
 - Need to qualify and ensure consistency in this adjustment factor.
- **Option 2:** Use the Rasnik alignment system to be installed and tested by SLAC.
- **Option 3:** Use optical viewports through vacuum and liquid nitrogen to directly measure fiducials on the accelerator.
 - Unclear if this is even possible and requires additional experimentation.



Mechanical Features – Alignment and Fiducials

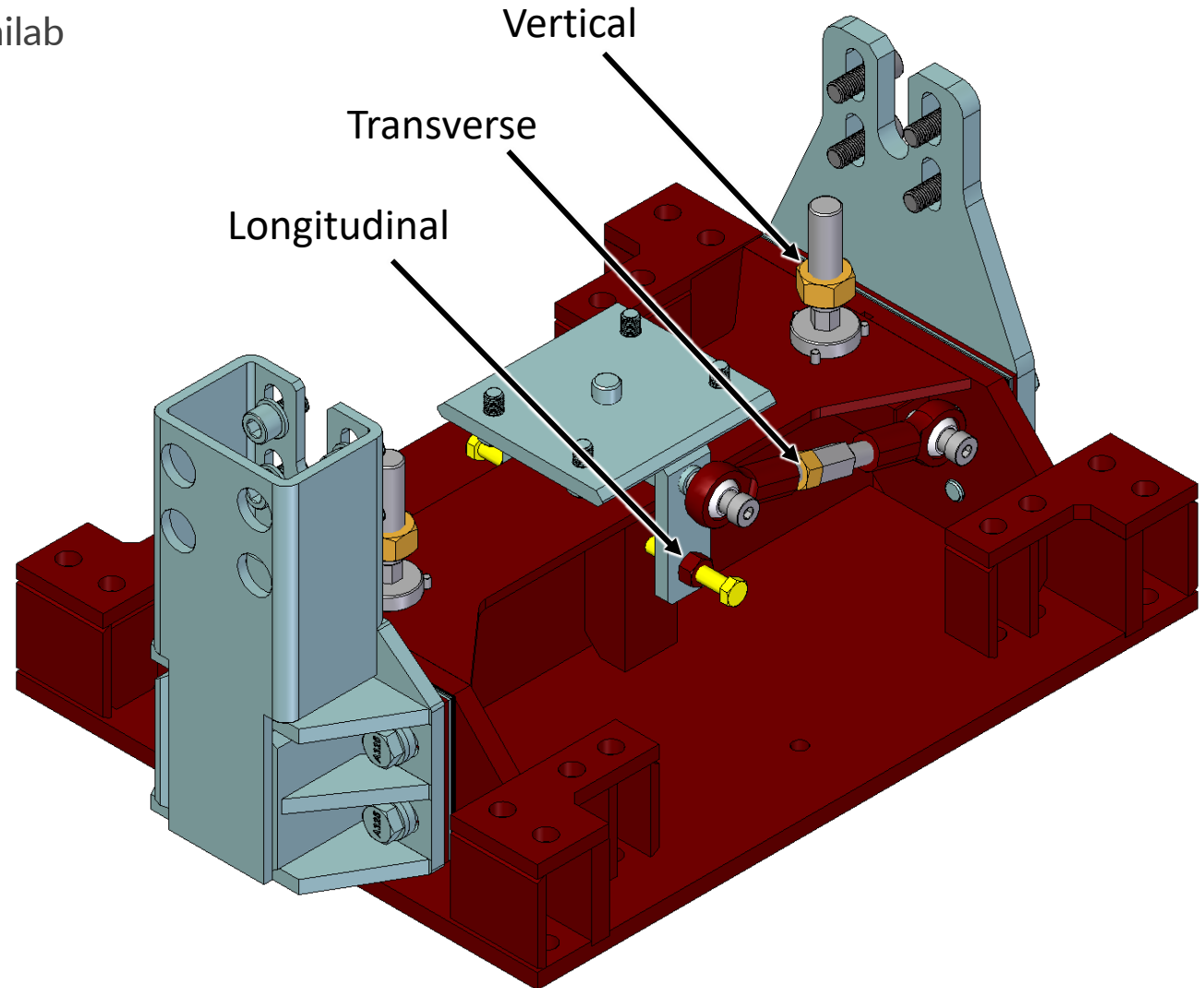
Actions

1. ESRF: Finalize mechanical alignment accuracy required before switching to beam-based alignment.
2. SLAC: Perform small-scale tests of measurement through windows and LN2.
3. SLAC: Investigate alternative alignment methods.
4. SLAC: Propose a plan for qualifying the alignment method chosen to ESRF's needs.



External Mounts

- Adjustable mounts were originally designed by Fermilab for the LCLS-II LINAC cryomodules.
- Allow for vertical, transverse, and longitudinal adjustment.
- Include additional seismic restraints on the sides.



Cryogenic and Vacuum Requirements

- LN used on cooling fill: **1400 L**
 - Vessel volume: 550 L
 - Cooling the structure: ~720 L
 - Loss during fill: ~100 L (over 12 hours)
- Standby losses: **133 L/24 hr** for 286 W standby power loss
 - Radiation: ~247 W
 - Conduction: ~38 W
 - Convection: 0 W (assuming $<1 \times 10^{-5}$ torr vacuum)
- Operating losses will vary and be in addition to the above.
- Vacuum
 - Primary concern is to maintain vacuum $<5 \times 10^{-5}$ torr to ensure no convection heat loss.
 - This vacuum level requires turbo pumps (and appropriate backing pumps), but the exact size of pumps depends on system outgassing and leak rates, which will be determined during testing at SLAC.

Conclusion